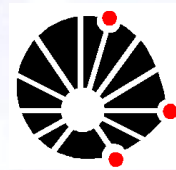


# In Situ Aging Characterization of Ti Alloys Using High Temperature X-Ray Diffraction



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***Brazil***



***5<sup>th</sup> International Conference on Diffusion in Solids and Liquids***  
***24 – 26 June 2009***  
***Rome, Italy***

# Outline

- Introduction
  - Orthopedic Implants
  - Total Hip Replacement / THR Requirements
  - Bone Elastic Deformation / Implant Elastic Modulus
  - Ti Alloys Phase Transformations
- Objectives
- Experiments
- Results
  - High Temperature X-Ray Diffraction
  - DSC
  - Aging Heat Treatment and Mechanical Behavior
  - Cold Forged Femoral Stem
- Conclusions

# Introduction

- **Concept of implanting materials in the human body is not new**

- **Ancient Egypt**

mummified foot with an artificial wooden toe



- **Ancient Egypt**

dental implant

in mummies



- **Ancient mediterranean civilization**

dental bridge

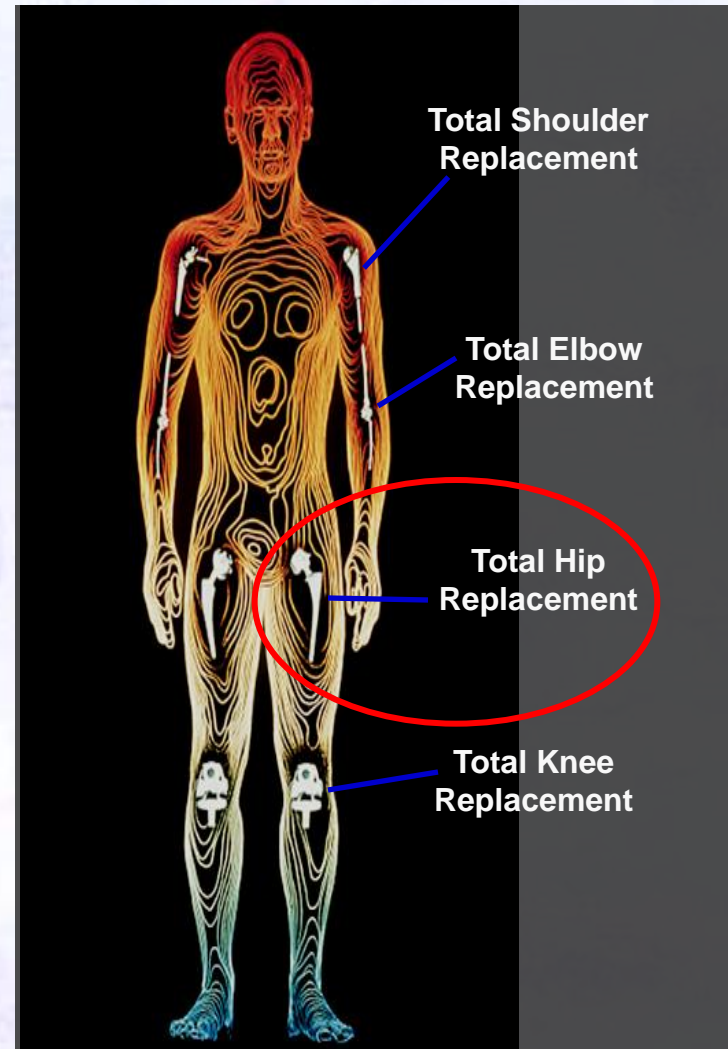


# Orthopedic Implants

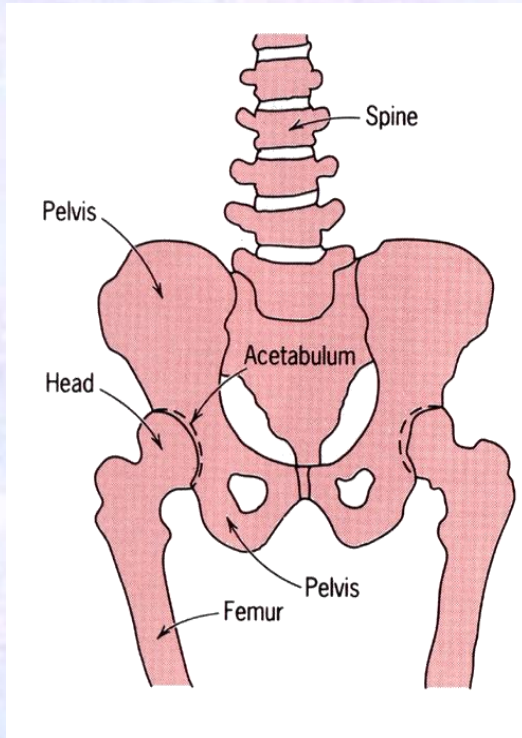
- Orthopedic biomaterials are successful in restoring mobility and quality life to millions of individuals each year
- Success of orthopedic biomaterials may be exemplified by their world market:
  - Annual growth rate of 7% to 9%
  - 2002 Sales of US\$ 14 billion
  - Joint replacements: US\$ 12 billion
    - Hip implant products: 2.5 billion  
(700,000 knee replacement surgeries)
    - Knee implant products: US\$ 2.5 billion  
(700,000 knee replacement surgeries)

# Total Joint Replacement

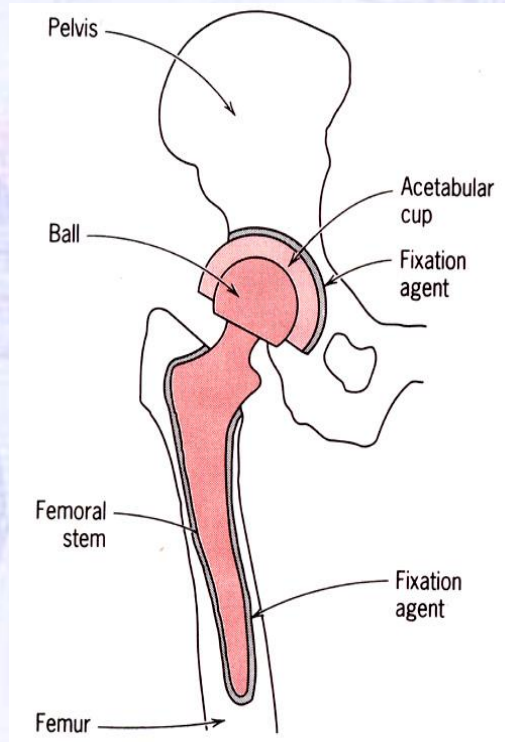
- **TJR** is a surgical procedure in which certain parts of an arthritic or damaged joint, are removed and replaced with a plastic or metal device called a prosthesis
- Prosthesis is designed to enable the artificial joint to move just like a normal, healthy joint.



# Total Hip Replacement



**Hip joints and adjacent skeletal components**



**Total hip replacement**



**Implant after surgery**

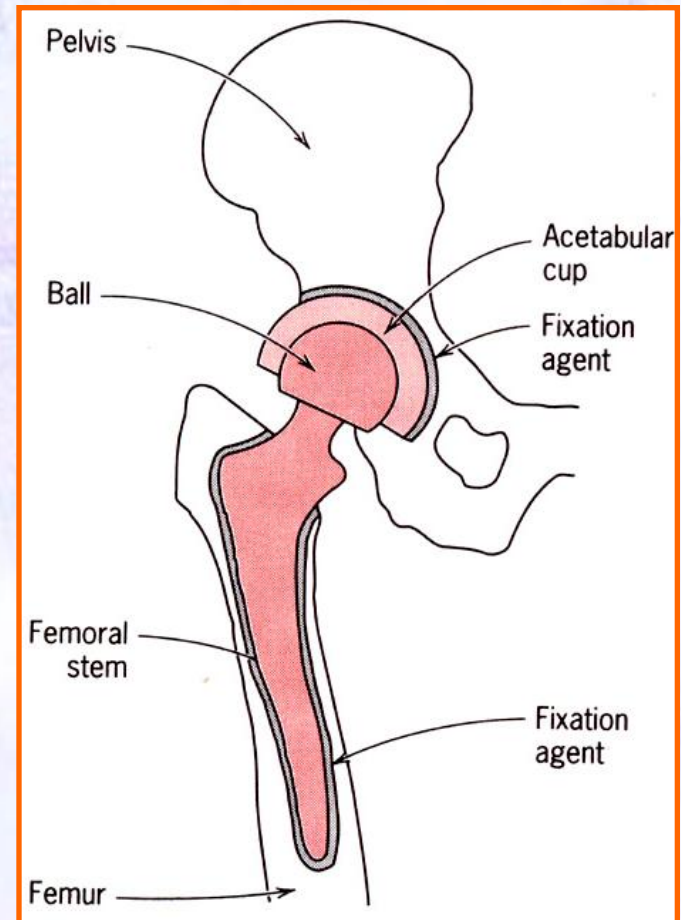
# THR Requiriments

- Biomaterials must show the following properties:

- High mechanical strength
- Processability
- Low prices
- High biocompatibility
- High corrosion resistance
- Must simulate bone elastic behavior

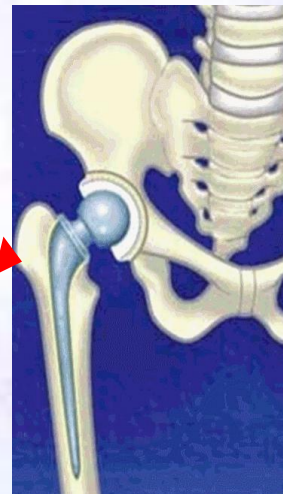
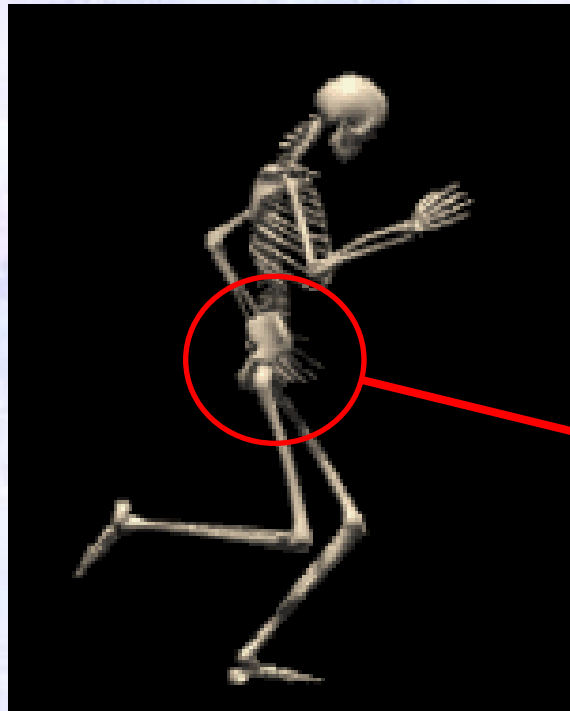
→ **low elastic modulus**

- $E_{\text{stainless steel}}$ : 200 GPa
- $E_{\text{Co-Cr-Mo Alloys}}$ : 230 GPa
- $E_{\text{Ti-CP}}$ : 110 GPa
- $E_{\text{Ti-6Al-4V}}$ : 106 GPa
- $E_{\beta\text{-alloys}}$ : <60 GPa
- $E_{\text{bone}}$ : 10 - 30 GPa



# Bone Elastic Deformation

- Implant material must simulate bone elastic behavior
- Insufficient load transfer from the implant to the bone causes bone re-absorption and loosening of the implant device
- Reduction of load applied to the bone causes bone mass loss and osteoporosis



## Bone fracture



Stainless  
steel 316L  
 $E = 200 \text{ GPa}$

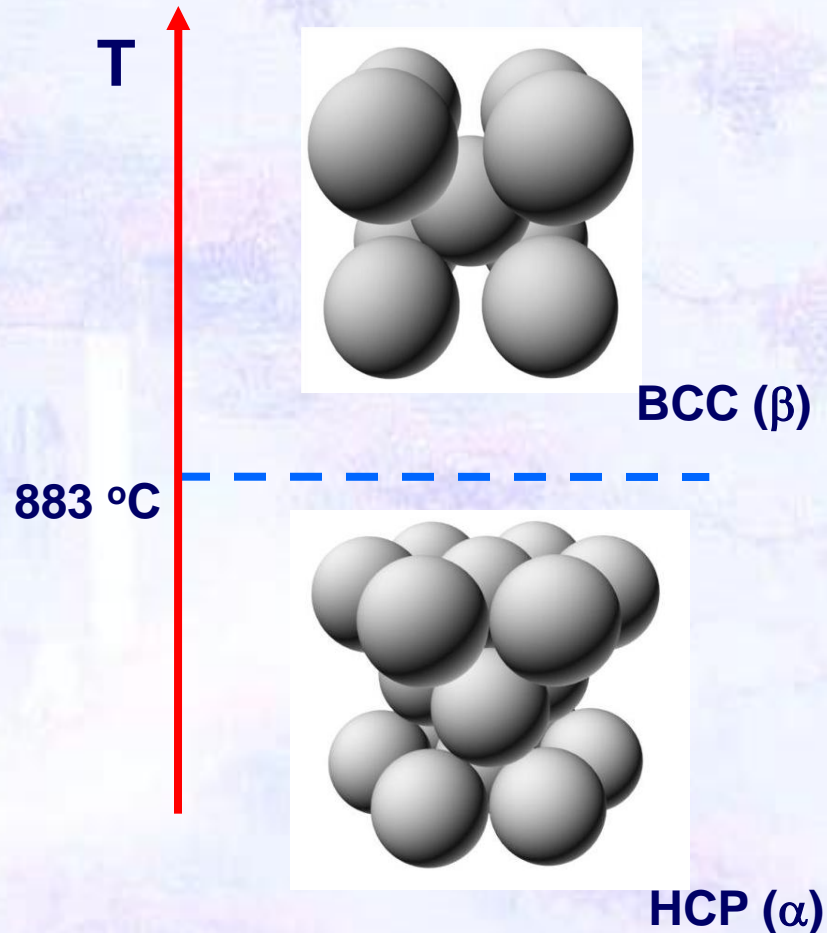


# Objectives

- The main aim of this research is to investigate  $\beta$  titanium alloys to be used as orthopedic biomaterials
- This work attempts to examine phase transformations during aging heat treatment of  $\beta$  Ti-Nb alloys with Sn additions and to correlate microstructure and mechanical behavior using high temperature X-ray diffraction.

# Titanium Metallurgy

- Titanium shows two allotropic forms: HCP and BCC
- Addition of alloy elements may change the phase stability and hence, the microstructure and mechanical behavior



# $\beta$ Titanium Alloy

## $\beta$ Ti alloys

$\beta$  Stabilizer elements:  
Cr, Nb, V, Ta, Mo

**HIGH STRENGTH-TO-DENSITY RATIO**

**LOW ELASTIC MODULUS**

**HIGH STRENGTH**

**HIGH TOUGHNESS**

**BIOCOMPATIBILITY**

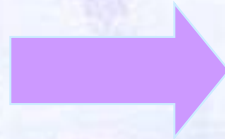
**EASY TO HEAT TREAT**

**EXCELLENT CORROSION RESISTANCE**

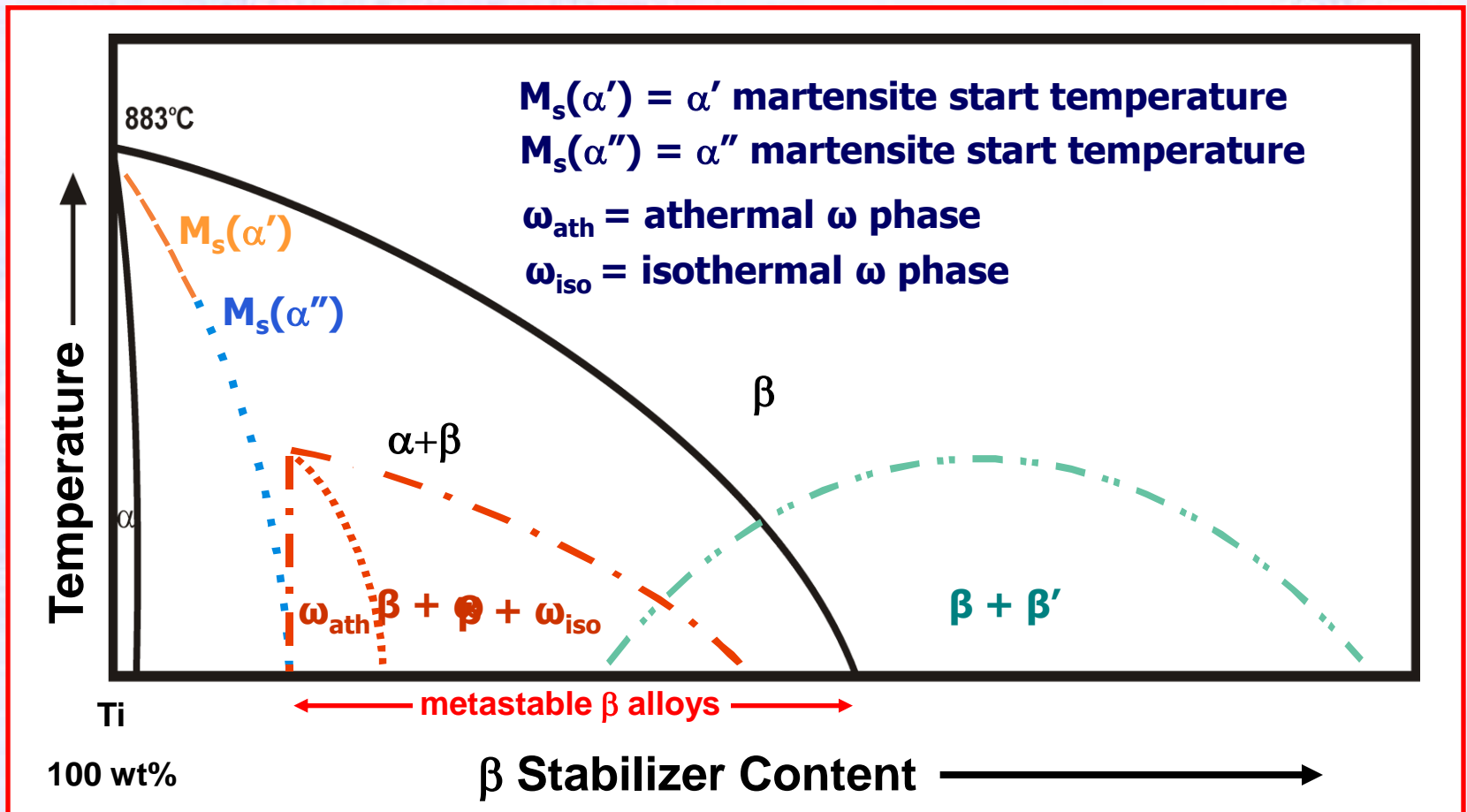
**LOW FORGING TEMPERATURE**

# Ti Alloys Phase Transformations

MECHANICAL  
 PROPERTIES OF Ti  
 ALLOYS

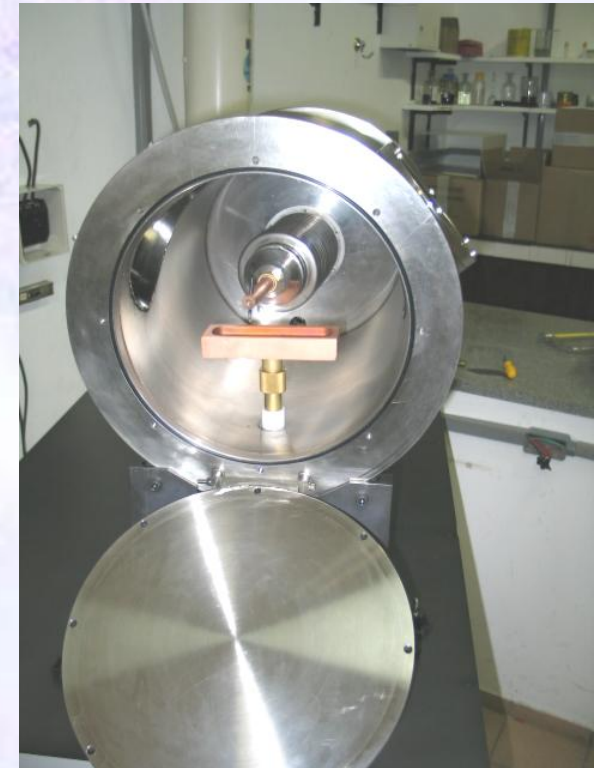
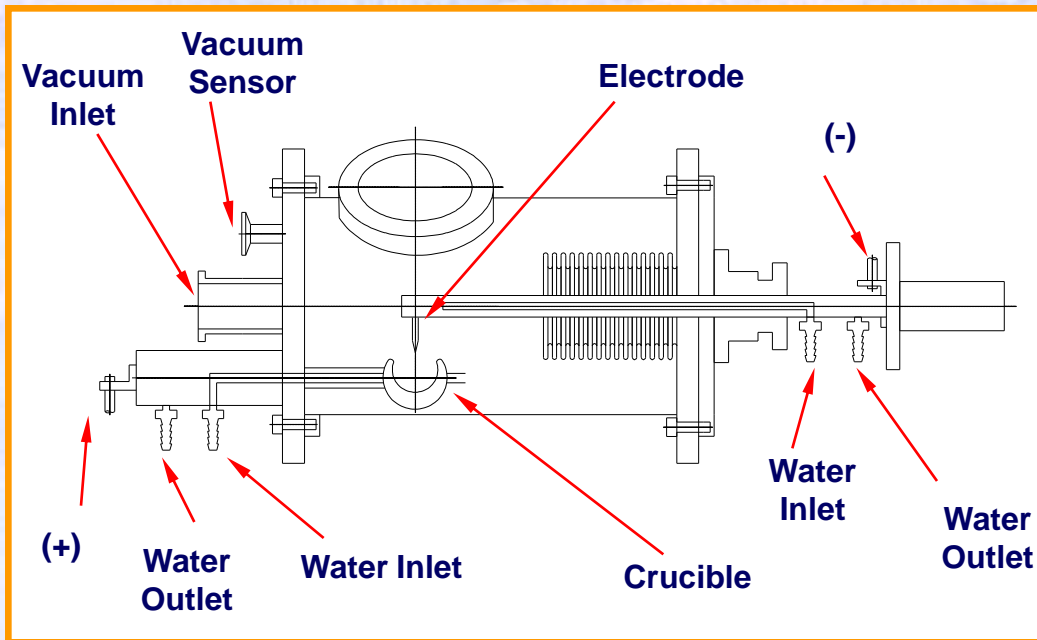


CHEMICAL COMPOSITION  
 MICROSTRUCTURE



# Alloy Preparation

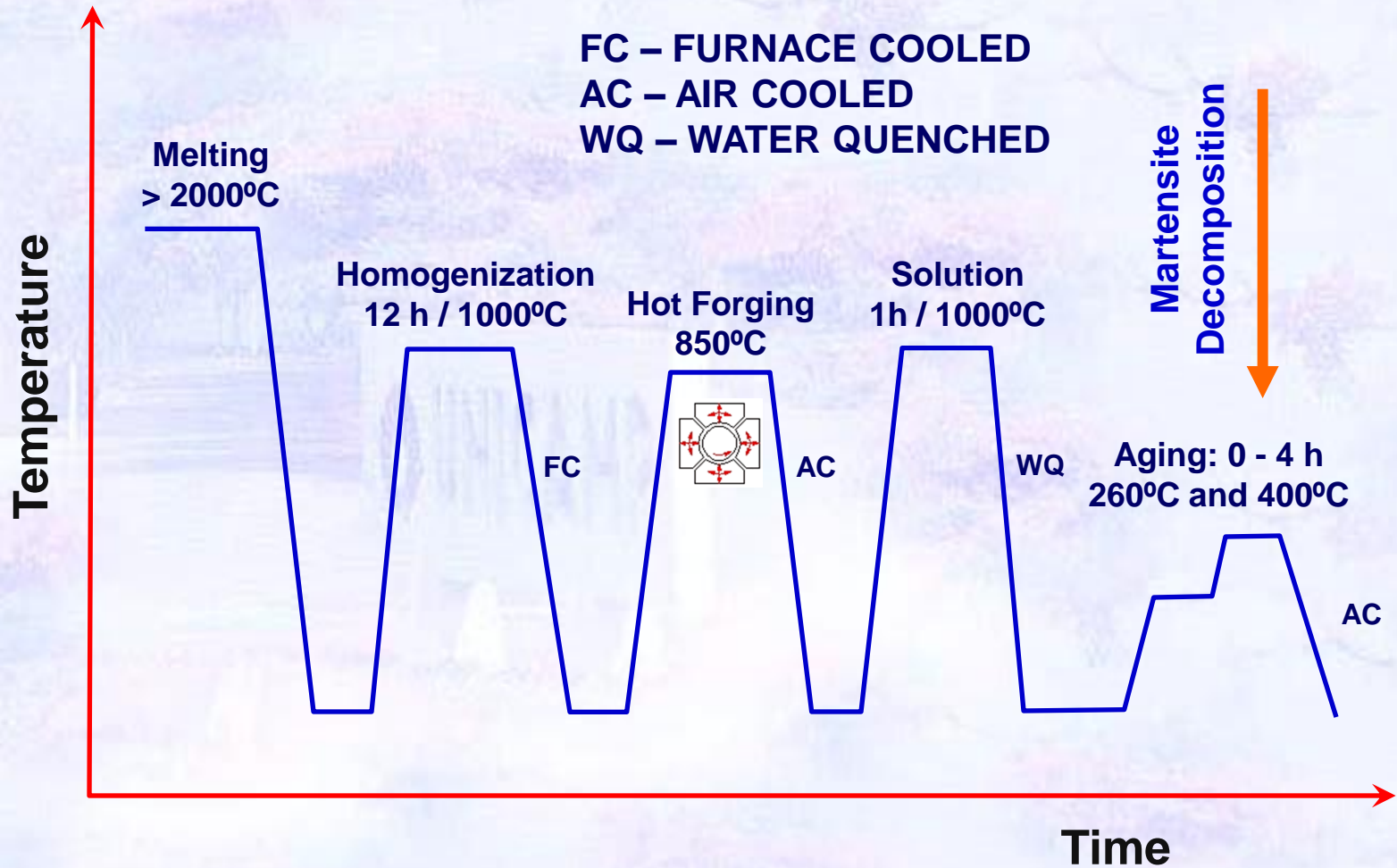
- Alloys were prepared by using high purity Ti, Nb and Sn
- Alloys were melted in arc furnace with non-consumable W electrode and water cooled copper hearth under Ar atmosphere



# Alloy Composition

<b>Nominal (%wt)</b>	<b>Measured (%wt)</b>
<b>Ti-30.0Nb</b>	<b>Ti-30.4Nb</b>
<b>Ti-30.0Nb-2.0Sn</b>	<b>Ti-30.5Nb-2.1Sn</b>
<b>Ti-30.0Nb-4.0Sn</b>	<b>Ti-30.6Nb-1.9Sn</b>

# Processing Route



# Sample Characterization

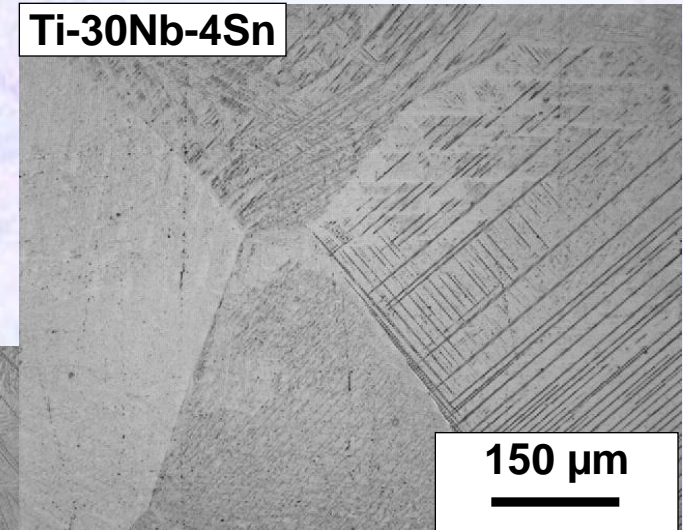
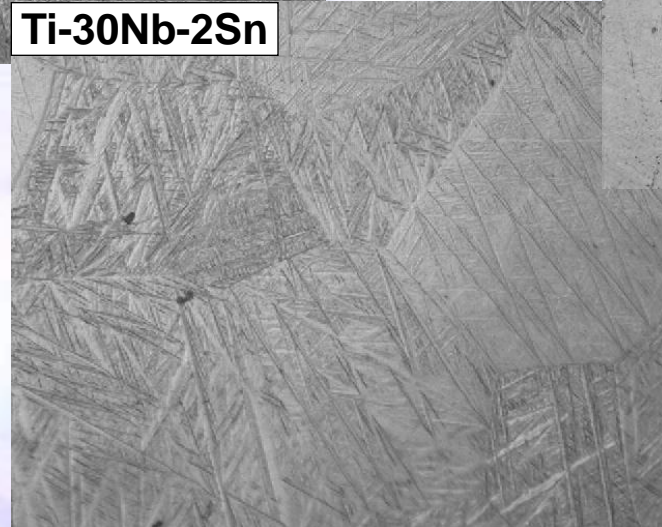
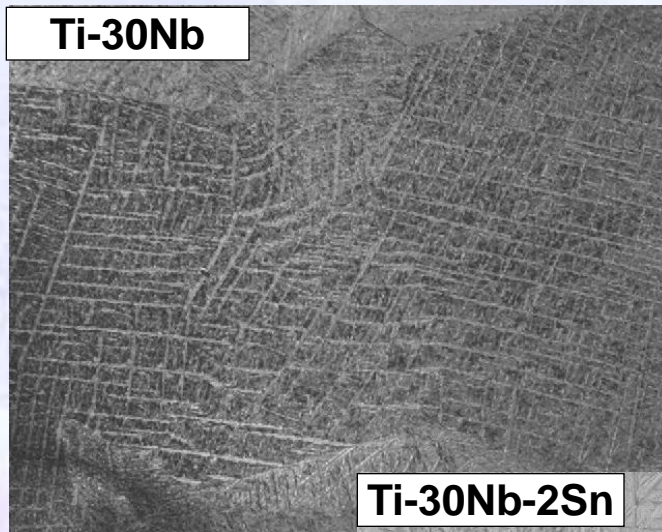
- Alloys chemical composition: X-ray fluorescence spectrometry
- Phase transformations : differential scanning calorimetry
- Phase detection: X-ray diffraction
- Phase evolution (Aging): high temperature X-ray diffraction
- Metallographic preparation: mechanical grinding using SiC sandpaper up to 1200 mesh, polishing with 6 and 1  $\mu\text{m}$  diamond paste
- Samples were etched in a Kroll's solution:  
5 % vol HF, 30 % vol  $\text{HNO}_3$  and 65 % vol  $\text{H}_2\text{O}$



# Effect of Sn on $\alpha''$ Amount

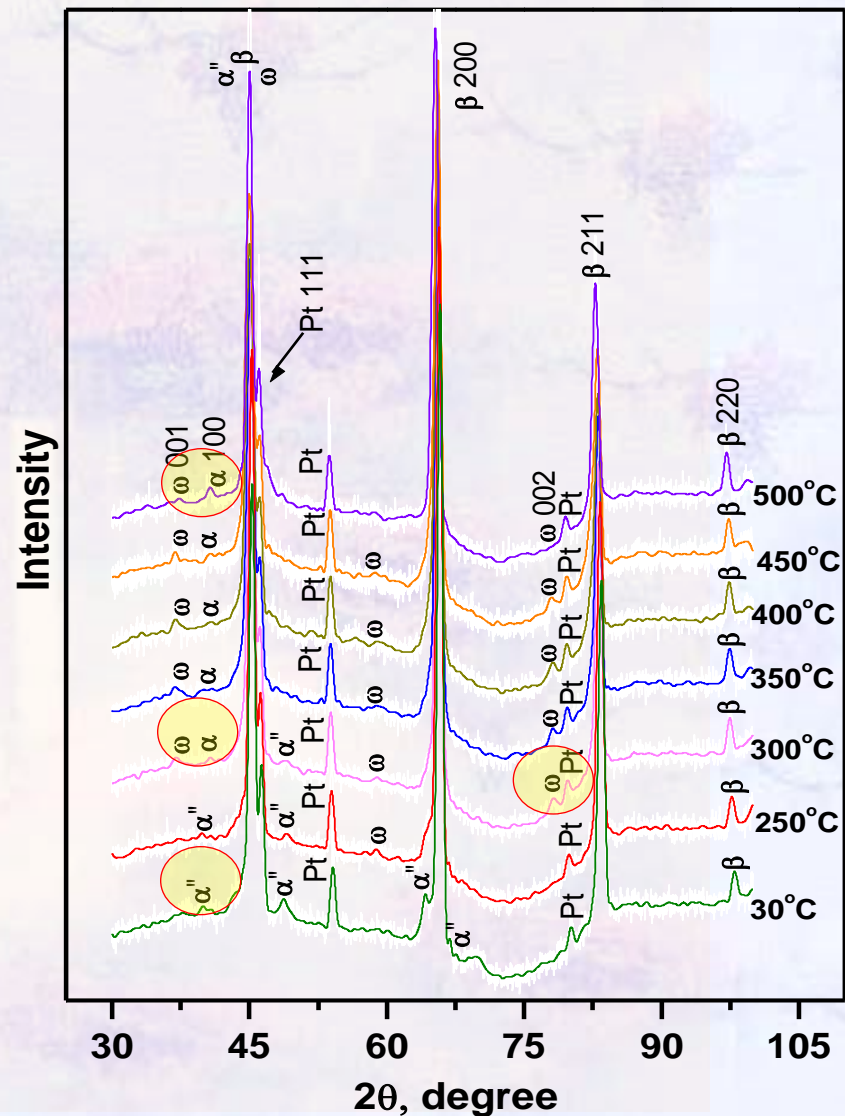
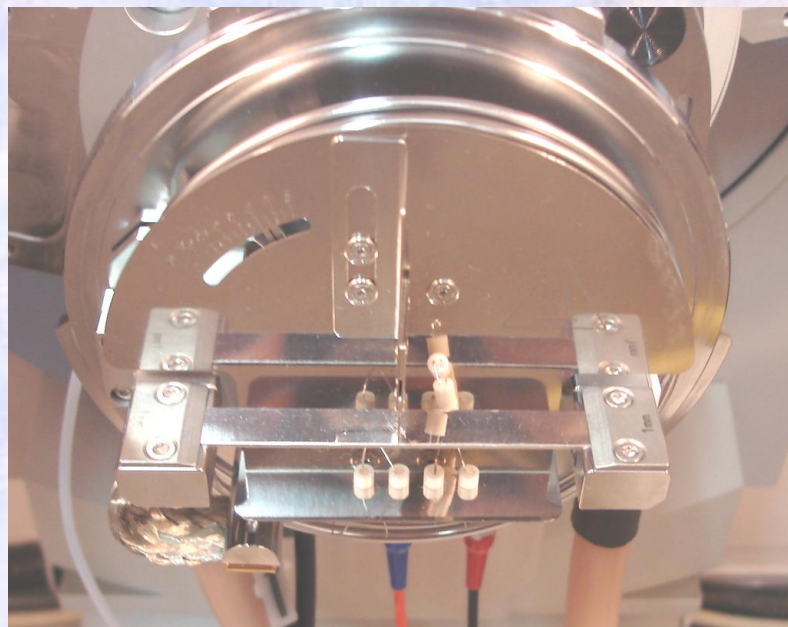
Effect of Sn addition on the amount of martensite

Water Quenched Samples



# $\alpha''$ Decomposition

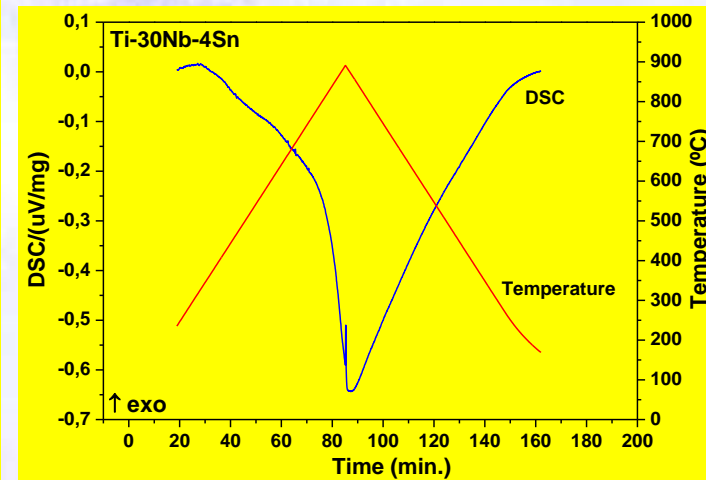
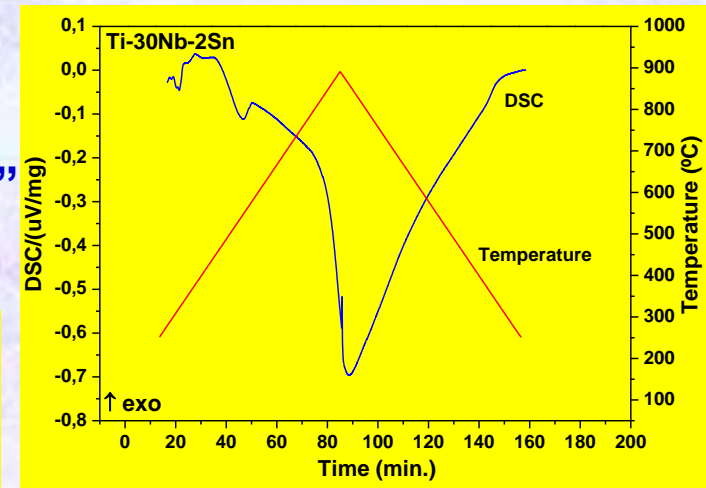
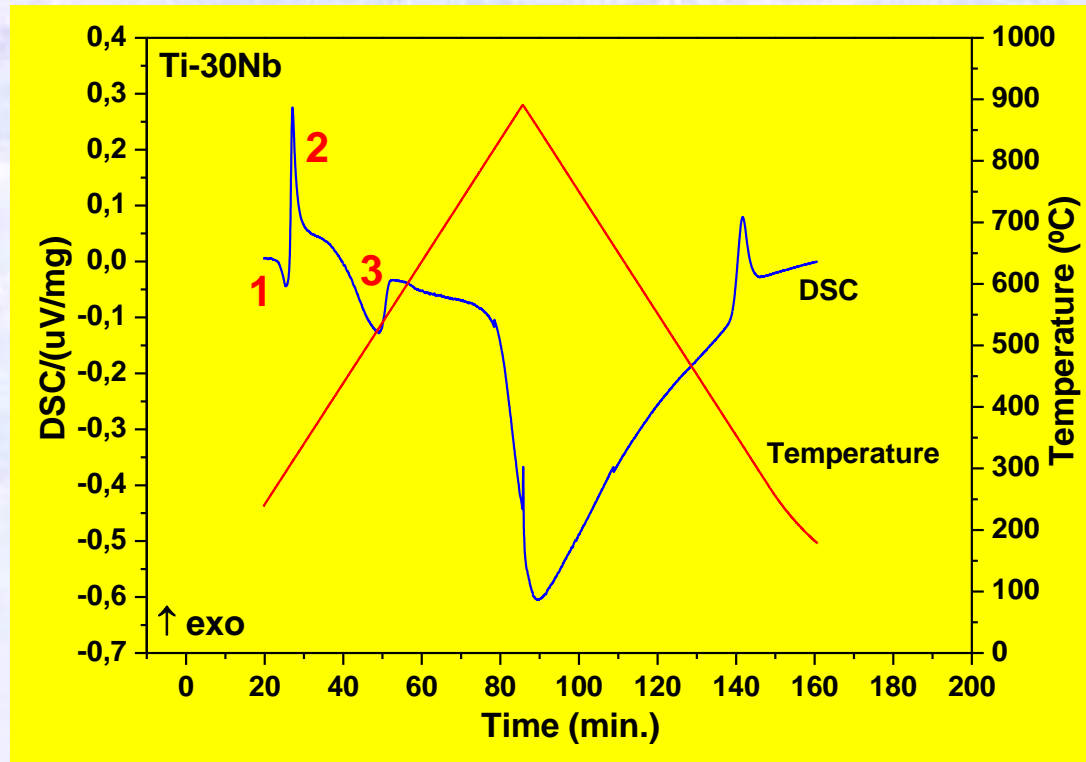
**In Situ Aging Characterization of Ti Alloys Using High Temperature X-Ray Diffraction**  
 $K\alpha$  Co:  $\lambda=0.17890$  nm



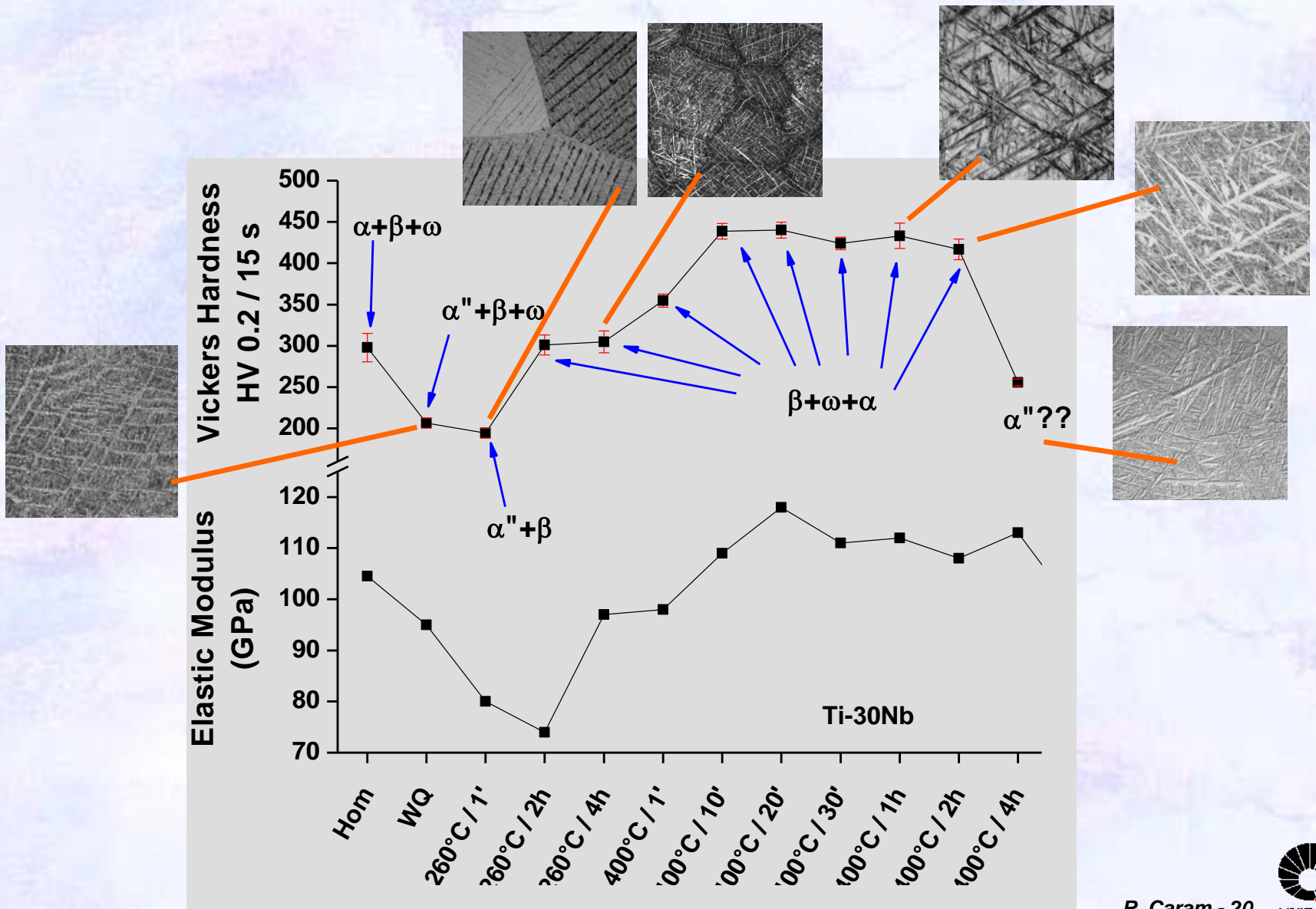
# $\alpha''$ Decomposition

## Thermal Analysis – DSC

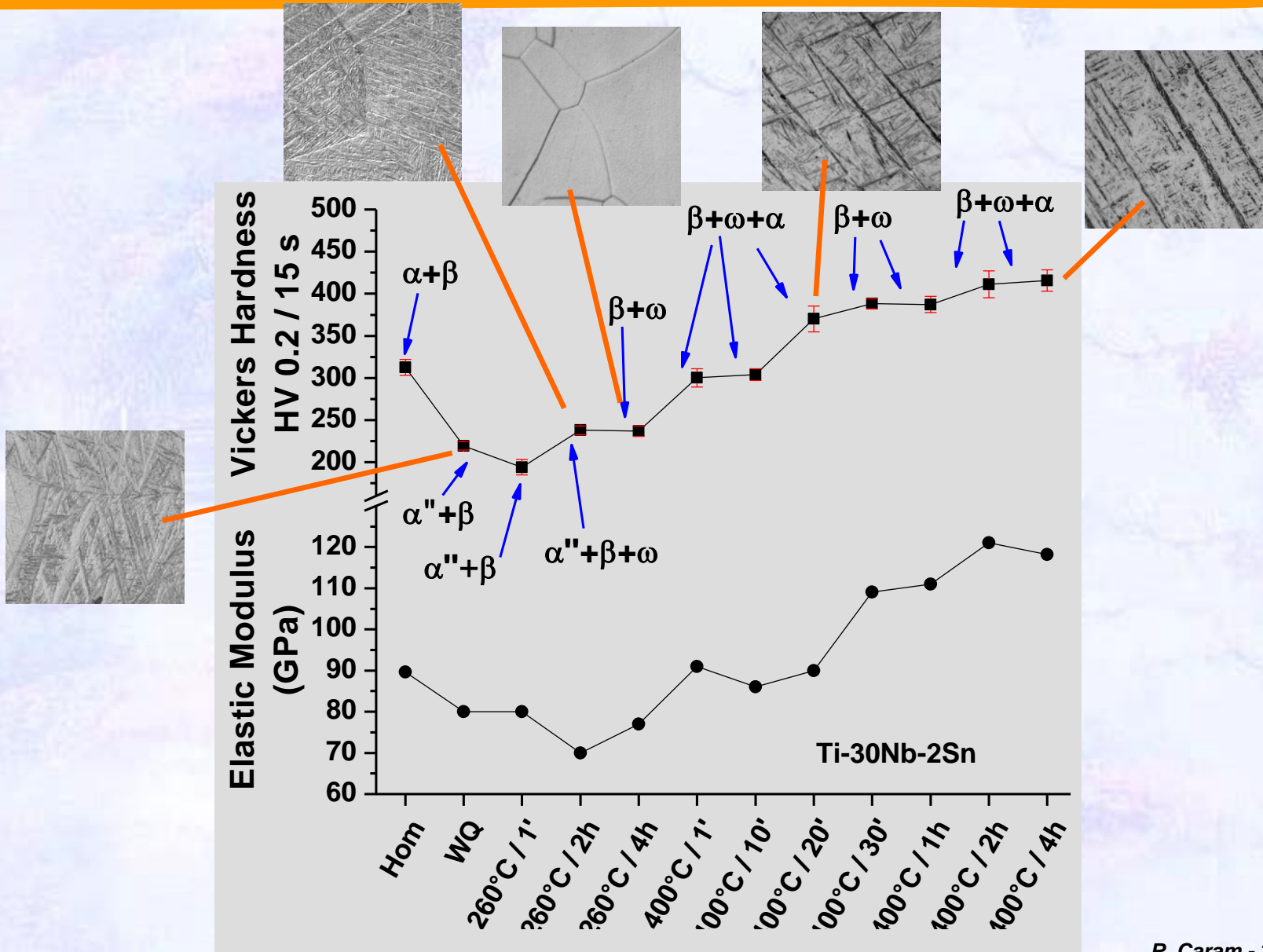
- WQ Ti-30Nb sample with  $\alpha''$  and  $\beta$  phases
- Peak 1: reverse transformation  $\alpha'' \rightarrow \beta$
- Peak 2: nucleation of  $\omega$  in  $\beta$  matrix (end of peak 1)
- Peak 3: nucleation of  $\alpha$  - " $\omega$  act as substrates"
- Peak 4:  $\beta$  transus



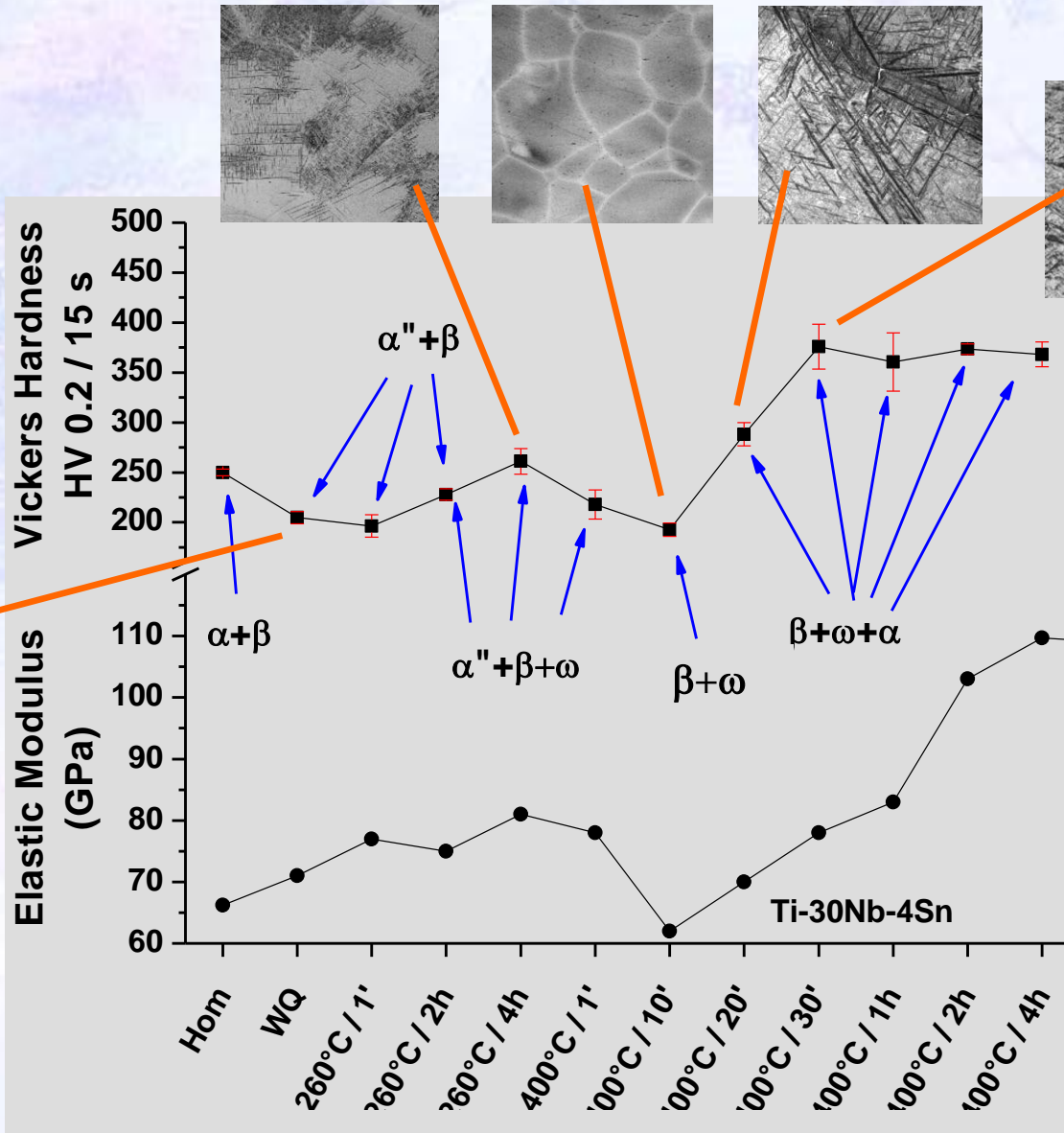
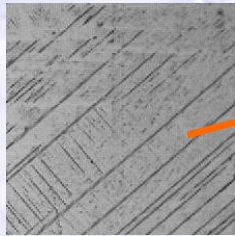
# Mechanical Behavior



# Mechanical Behavior



# Mechanical Behavior



# Tensile Test: Mechanical Properties

## Effect of aging on mechanical behavior

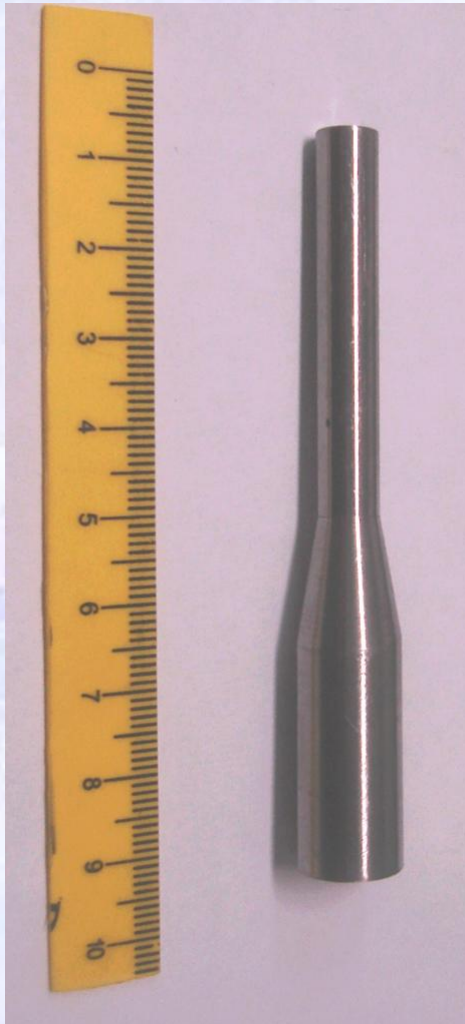
Alloy Condition	Phases (XRD)	$\sigma_{UTS}$ (MPa)	Elong (%)	E (GPa)	Hardness (HV)
Ti-30Nb Full $\beta$	$\beta + \omega$	$532 \pm 21$	$30 \pm 7$	74	$199 \pm 6$
Ti-30Nb Aged	$\beta + \alpha + \omega$	$826 \pm 24$	$0.8 \pm 0.1$	105	$424 \pm 10$
Ti-30Nb-2Sn Full $\beta$	$\beta$	$500 \pm 32$	$36 \pm 4.0$	70	$219 \pm 5$
Ti-30Nb-2Sn Aged	$\beta + \alpha + \omega^*$	$857 \pm 22$	$0.8 \pm 0.2$	100	$432 \pm 15$
Ti-30Nb-4Sn Full $\beta$	$\beta$	$531 \pm 20$	$21.6 \pm 1.2$	62	$211 \pm 7$
Ti-30Nb-4Sn Aged	$\beta + \alpha + \omega^{**}$	$937 \pm 18$	$1.2 \pm 4.3$	101	$387 \pm 11$

$\omega^*$  - small amount

$\omega^{**}$  - very small amount

# Cold Forging

## Cold Forged Femoral Stem using Ti-30Nb-4Sn alloy





# Optimized Mechanical Behavior

- **Problem:** When using aging process, it is virtually impossible to obtain a  $\beta$  Ti alloy with high mechanical strength and low elastic modulus
- **Solution:** Application of different heat treatment procedures according to the region of the prosthesis



# Conclusions

- In WQ condition (1h/1000°C/WQ) the microstructure of Ti-30Nb, Ti-30Nb-2Sn and Ti-30Nb-4Sn alloys was formed by  $\beta$  and  $\alpha''$  phase and the amount of  $\alpha''$  decreases with increase of Sn;
- Aging procedure allowed to verify that  $\alpha''$  decomposition results in precipitation of  $\beta$ ,  $\omega$  and finally,  $\alpha$  phases;
- Results suggest that Sn may act as a suppressor of  $\omega$  phase precipitation, which allows the control of microstructure features and hence, mechanical properties
- While rapid quenched Ti-Nb-Sn samples showed yield strength below 310 MPa, which makes easier cold forging process, whose aged sample value increased up to 900 MPa
- Full  $\beta$  alloy showed elastic modulus below of 62 GPa
- These final values are very suitable in terms of orthopedic biomaterial applications

**Questions??**